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2.004 Dynamics and Control II  
Spring 2008

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MASSACHUSETTS INSTITUTE OF TECHNOLOGY  
DEPARTMENT OF MECHANICAL ENGINEERING

2.004 *Dynamics and Control II*  
Spring Term 2008

Problem Set 4

Assigned: Feb. 29, 2008

Due: March 7, 2008

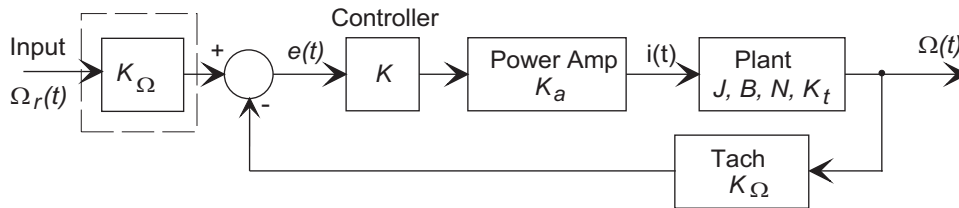
**Reading:**

- 2.004 Class Handout: *Introduction to the Operational Amplifier*

**Problem 1:**

Do this problem before your Lab 3 session and take your solution with you.

In Lab 3 you will be designing and implementing a closed-loop controller to regulate the angular velocity of the copper flywheel. In Lab 2 you measured the characteristics of the system components. This problem asks you to predict the closed-loop behavior of the system, so that you may compare your predicted and measured behavior in the lab:

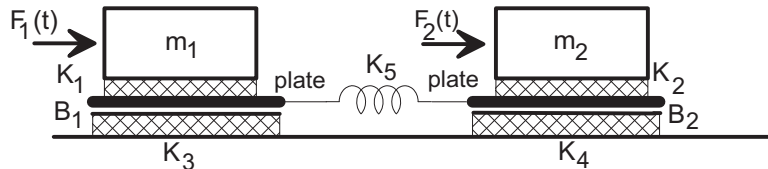


- (a) Derive the transfer function relating the angular velocity  $\Omega$  of the motor to the voltage input command in terms of the controller gain  $K$ , servo amp gain  $K_a$ , motor torque constant  $K_t$ , and tachometer gain  $K_\Omega$ . Ignore nonlinearities such as Coulomb friction. (Question: Why did I include the block  $K_\Omega$ , in the input?)
- (b) Now put in numerical values:
- You computed the value of  $J$ .
  - The motor-drive gears have 44 and 180 teeth.
  - The value of  $K_a = 2$  amps/volt. The value of  $K_\Omega = 0.016$  v/rpm.
  - Assume a value  $K = 3$  for the controller.
  - We will start with one damping magnet. From Lab. 1, an average over several groups for the damping with one magnet was  $B = 0.014$  N.m.s/rad.
- (b) With all of the numerical values substituted, except for the controller gain  $K$ , derive the closed loop time-constant in terms of  $K$ .

(c) Similarly, determine the steady-state error to a constant (step) input as a function of the controller gain  $K$ .

**Hint:** You may find certain similarities between this problem and the automobile cruise control example we discussed in class.

**Problem 2:** A parts assembly station on a production line exhibits a severe vibration problem. A simplified schematic representation is shown below:

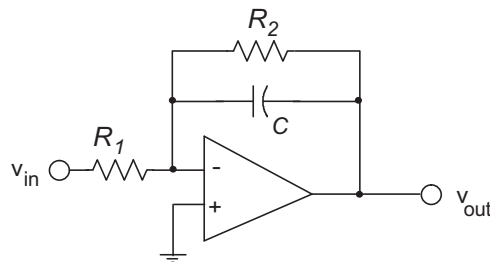


Two large tables of mass  $m_1$  and  $m_2$  are each mounted to a sliding metal plate on resilient rubber mounts, with shear stiffness  $K_1$  and  $K_2$  as shown. The tables are each subjected to a vibrational excitation force,  $F_1(t)$  and  $F_2(t)$ . The plates are able to slide viscously on a second pair of deformable rubber mounts, with shear stiffness  $K_3$  and  $K_4$  as shown. The viscous sliding coefficients are  $B_1$  and  $B_2$ . The two plates are coupled by a shaft with longitudinal stiffness  $K_5$ .

- Draw a linear graph for the system using the two forces  $F_1$  and  $F_2$  as inputs.
- Write continuity (force balance) equations for each of the nodes on your graph. (You don't have to consider the reference node.)
- Using the elemental impedances/admittances substitute the component values and generate a set of simultaneous algebraic equations in the nodal velocities.

**Do not** attempt to solve the equations.

**Problem 3:** The op-amp circuit shown below is commonly used as a “filter” in control systems.



In the class handout we showed that the output of the standard inverting amplifier is

$$v_{out} = -\frac{R_f}{R_{in}} v_{in}$$

- (a) Extend the argument in the handout to show that for any impedance elements  $Z_f$  and  $Z_{in}$  the output may be written

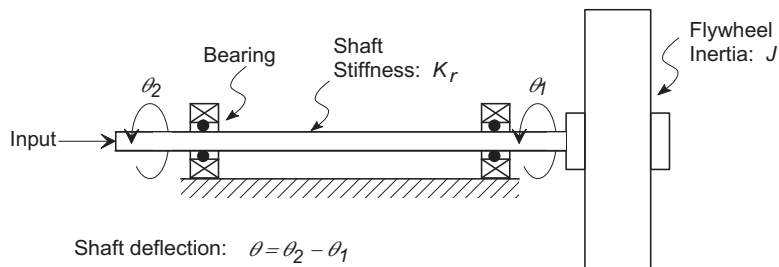
$$V_{out}(s) = -\frac{Z_f}{Z_{in}} V_{in}(s).$$

- (b) Find the transfer function  $V_{out}(s)/V_{in}(s)$  for the circuit above.  
 (c) Find the differential equation relating  $v_{out}(t)$  to  $v_{in}(t)$ .  
 (d) If  $R_2 = 22 \text{ k}\Omega$  (22,000  $\Omega$ ),  $R_1 = 6.8 \text{ k}\Omega$ , and  $C = 0.47 \text{ }\mu\text{F}$ d (these are common values), find (i) The time-constant, and (ii) the steady-state output voltage  $v_{out}$  when the input is 2.5 v.

**Problem 4:** Nise Ch, 2, Prob. 30. For each system:

- (a) Draw the linear graph representation of the system.  
 (b) Write the equations of motion (as Nise requests) in the Laplace domain using the node equations. (Do not solve.)

**Problem 5:** Consider the rotational system shown below:



The torsional stiffness of a cylindrical shaft of diameter  $D$  and length  $l$  is

$$K_r = G \frac{\pi D^4}{32 l}$$

where  $G$  is the shear modulus of the shaft material. A steel shaft, 5 m long and 5 cm in diameter, drives a steel cylindrical flywheel with a 30 cm diameter and a thickness of 5 cm. Steel has a density of  $\rho = 7.8 \text{ gm/cm}^3$  and a shear modulus of  $G = 83 \text{ GPa}$ . Assume that each of the bearings exhibits a rotational viscous frictional coefficient  $B = 0.1 \text{ N-m-s/rad}$ . The input is an angular velocity source  $\Omega_s(t)$ .

As a controls engineer you have been asked to design a closed-loop controller to maintain the flywheel at a constant speed under varying load conditions. In order to do this you need a transfer function model of the plant:

- (a) What are the values of the shaft stiffness  $K_r$  and the flywheel moment of inertia  $J$ .  
 (b) Derive the transfer function (with numerical coefficients) relating the flywheel angular velocity  $\Omega_1$  to the input  $\Omega_s(t)$ .